



Substitute Specification

SPECIFICATION

5 SWIRL CHAMBER USED IN ASSOCIATION WITH A
COMBUSTION CHAMBER FOR DIESEL ENGINES

TECHNICAL FIELD

10 【0001】 The present invention relates generally to a combustion
chamber for diesel engines, and more particularly, to improvements
upon a swirl chamber used in association with a combustion
chamber for diesel engines.

BACKGROUND ART

15 【0002】 In general, diesel engines are notorious as a major source
of environmental contaminants such as NO_x and fumes. However,
no effective measures have been accomplished for solving those
problems. It is known that these problems are due to the
incomplete combustion in the engine occurring because of
inadequate mixing of air and fuel. To solve these problems,
20 swirl-aided combustion systems are commonly used. Here is one
example for tackling this problem, which is disclosed in Japanese
Patent Laid-open Application No. 07-97924. Referring to Fig. 10, the
known combustion chamber fitted with a swirl chamber will be
described:

25 【0003】 In Figs. 10A and 10B the right-hand side (toward the

central axis 103) is called "rearward", and the left-hand side (toward the cylinder liner 104) is "forward" each as designation for convenience only. The known combustion chamber shown in Fig. 10A is provided with a cylinder 101 having a cylinder head 105, a reciprocating piston 102, and a combustion chamber 109. In addition, the cylinder head 105 is provided with a recess 106 in which a mouthpiece 107 is fitted. The mouthpiece 107 is provided with a top-open recess 107a, and the recess 106 includes a bottom-open recess 106a. The top-open recess 107a and the bottom-open recess 106a constitute a space 108 functioning as a swirl chamber, hereinafter the space being referred to as "swirl chamber 108". The swirl chamber 108 communicates with the combustion chamber 109 through a main nozzle hole 111 having a center axis 113. The main nozzle hole 111 is forwardly inclined toward the swirl chamber 108. The mouthpiece 107 is additionally provided with a pair of sub-nozzle holes 112, through which a secondary air is forced into the swirl chamber 108 on the compression stroke. The sub-nozzle holes 112 are symmetrically positioned on opposite sides of the central axis 113-114 as shown in Fig. 10A.

【0004】 Under the construction mentioned above, however, a major disadvantage is that the second air ejected through the sub-nozzle holes 112 does not reach the central part of the swirl chamber 108, thereby failing to bring about effective swirls therein. In this way the conventional sub-nozzle holes 112 are not conducive to the full

5 【0009】 According to the present invention, a swirl chamber used
in association with a combustion chamber, wherein the combustion
chamber is defined by a piston, a cylinder, and a cylinder head,
includes a mouthpiece fitted in a hole of the cylinder head, the hole
10 having a bottom-open recess, and the mouthpiece including a
top-open recess, the bottom-open recess and the top-open recess
constituting a space for the swirl chamber; a main nozzle hole
produced through a base wall of the mouthpiece to allow the swirl
chamber to effect communication between the combustion chamber
15 and the swirl chamber; and a pair of sub-nozzle holes, which are
separated from the main nozzle hole, produced through the base
wall of the mouthpiece, the holes being positioned on opposite sides
of the central axis of the main nozzle hole when the mouthpiece is
seen from just above; wherein each of the sub-nozzle holes is
20 arranged to pass inside a hypothetical sphere depicted around a
center of an upper circle of the top-open recess and having a radius
of 70% of a diameter of the upper circle of the top-open recess.

BRIEF DESCRIPTION OF THE DRAWINGS

20 【0010】 Fig. 1 is generally a diagrammatic view exemplifying a
first embodiment of the present invention; Fig. 1A being a plan view,
Fig. 1B being a cross-sectional view taken along the line B-B of Fig.
1A; Fig. 1C being a bottom view, and Fig. 1D being a cross-sectional
view taken along the line D-D;

25 【0011】 Fig. 2 is generally a diagrammatic view exemplifying the

nozzle hole in the mouthpiece shown in Fig. 1; Fig. 2A being a vertical cross-sectional side view of the mouthpiece, Fig. 2B being a perspective view of the nozzle hole; Fig. 2C being a diagrammatic view of the nozzle hole viewed in the direction indicated by the
5 arrow C in Fig. 2A, and Fig. 2D being a bottom view of the nozzle hole;

【0012】 Fig. 3 is generally a diagrammatic view exemplifying the swirl chamber shown in Fig. 1; Fig. 3A being a horizontal cross-sectional plan view of a cylinder incorporating a piston, and
10 Fig. 3B being a cross-sectional side view of the swirl chamber and the surrounding part members;

【0013】 Fig. 4 is a graph showing NO_x content in the exhaust gases under the first embodiment shown in Fig. 3, in comparison with a contrasted example 1 having no sub-nozzle holes;

15 【0014】 Fig. 5 is a graph showing the amount of NO_x and fumes exhausted under the first embodiment shown in Fig. 3, in comparison with contrasted examples 1 and 2;

【0015】 Figs. 6 is generally a graph showing the relationship between the cross-sectional area of the sub-nozzle holes and the
20 characteristics of gases exhausted from the swirl chamber of Fig. 3; Fig. 6A showing variations in the amount of NO_x in relation to the cross-sectional area; Fig. 6B showing variations in the amount of fumes in relation to the cross-sectional area; and Fig. 6C showing variations in the total amount of NO_x and fumes in relation to the
25 cross-sectional area;

5 【0016】 Fig. 7 is generally a diagrammatic view exemplifying the
mouthpiece of a second embodiment; Fig. 7A being a plan view, Fig.
7B being a cross-sectional view taken along the line B-B in Fig. 7A;
Fig. 7C being a bottom view, and Fig. 7D being a cross-sectional
view taken along the line D-D in Fig.7B;

10 【0017】 Fig.8 is generally a diagrammatic view exemplifying the
mouthpiece of a third embodiment; Fig. 8A being a plan view, Fig.
8B being a cross-sectional view taken along the line B-B in Fig. 8A;
Fig. 8C being a bottom view, and Fig. 8D being a cross-sectional
view taken along the line D-D in Fig.8B;

15 【0018】 Fig. 9 is generally a diagrammatic view exemplifying the
mouthpiece of a fourth embodiment; Fig. 9A being a plan view, Fig.
9B being a cross-sectional view taken along the line B-B in Fig. 9A;
Fig. 9C being a bottom view, and Fig. 9D being a cross-sectional
view taken along the line D-D in Fig.9B; and

 【0019】 Fig. 10 is generally a diagrammatic view exemplifying a
known swirl chamber; Fig. 10A being a plan view of the mouthpiece
and the piston, and Fig. 10B being a vertical cross-sectional side
view of a swirl chamber and surrounding part members.

20 DESCRIPTION OF PREFERRED EMBODIMENTS

 【0020】 Throughout the drawings like numerals are used to
designate like components, and in Figs. 1B, 3B, 7B, 8B, 9B, and 2A
the right-hand side is “forward”, and the left-hand side is
“rearward” for convenience of illustration only. A first embodiment
25 is shown in Figs. 1 to 6, in which a pair of sub-nozzle holes 12 are

provided upright in parallel with the central axis 3 of a cylinder 1. This is the same with a second embodiment shown in Fig. 7, but in the third embodiment shown in Fig. 8 and a fourth embodiment shown in Fig. 9 the sub-nozzle holes 12 are slightly converged and slightly diverged toward their top open ends, respectively. The feature common with all the embodiments is that the sub-nozzle holes are spaced from, and positioned symmetrically on opposite sides of, the main nozzle hole. In addition, the sub-nozzle holes are produced on the forward side.

10 **【0021】** In Fig. 3B a reciprocating piston 2 is provided inside a cylinder 1 along whose central axis 3 the piston 2 moves up and down. The cylinder 1 has a head 5 having a recess 6 in which a mouthpiece 7 is fitted. The recess 6 includes a bottom-open recess 6a, and the mouthpiece 7 includes a top-open recess 7a. The

15 bottom-open recess 6a and the top-open recess 7a constitute a space 8 that is utilized as a swirl chamber. The cylinder 1 is provided with a combustion chamber 9 having a main nozzle hole 11 passing through the mouthpiece 7. The combustion chamber 9 and the swirl chamber 8 communicate with each other through the main

20 nozzle hole 11, which is forwardly inclined toward the swirl chamber 8 from the combustion chamber 9, as shown in Fig. 3B. The mouthpiece 7 has an undersurface 7d in a plane perpendicular to the central axis 3 of the cylinder 1.

25 **【0022】** As best shown in Fig. 3B, a fuel jet nozzle 19 and a heat plug 20 are provided toward the swirl chamber 8. The piston 1 is

provided with a triangular recess 21 adapted to guide a gas flow,
wherein the root portion of the recess 21 is positioned immediately
below the main nozzle hole 11, and as best shown in Fig. 3A, the
recess 21 expands progressively far from the main nozzle hole 11,
5 thereby having a diminishing depth, as best shown in Fig. 3B.

【0023】 The principle underlying the combustion chamber 9 fixed
with the swirl chamber 8 is as follows:

On the compression stroke the piston 2 rises, thereby
introducing compressed air into the swirl chamber 8 to cause swirls
10 therein. When the piston 2 reaches the top dead point, fuel is
ejected through the ejection nozzle 19. The fuel is mixed with the
air in the swirl chamber 8, and the charge of fuel and air is ignited,
and burned in the chamber 8, and as a result, it expands in volume.
The expanded gases pass into the combustion chamber 9 through
15 the main nozzle hole 11. The fresh charge expands and rises as it
goes away from the main nozzle hole 11 in the triangular recess 21.
The fuel content in the fresh charge mixes with air in the
combustion chamber 9, and the mixture is ignited and burned.

【0024】 The sub-nozzle holes 12 will be described:

20 In Figs. 1A to 1D, particularly in Figs. 1B and 1D, the
sub-nozzle holes 12 are provided in pair through a base wall 10 of
the mouthpiece 7. Each of the sub-nozzle holes 12 is away from the
main nozzle hole 11 such that they are symmetrically positioned
about the central axis 13 of the main nozzle hole 11 or about its
25 extension 14, depending upon the shape of the main nozzle hole 11.

5 【0025】 Figs. 1A, 1B, and 1D show a hypothetical sphere 15 about
a center 7c which is the center of the open end 7b of the recess 7a.
The radius of the open end 7b is supposed to be 100%, and that of
the sphere 15 to be 50%. Each of the sub-nozzle holes 12 is
positioned such that its central axis 12a-12b passes through the
sphere 15, or in the drawing, through the sphere 15.

10 【0026】 Preferably, the radius of the sphere 15 is 70%; more
preferably, 60%, and most preferably, 50%. In Figs. 1A, 1B, and 1D
the innermost, middle, and outermost sphere 15 are drawn in
correspondence to 50%, 60%, and 70%, respectively. It has been
demonstrated that this range of angular positioning of the
sub-nozzle holes 12 enables a secondary air to gather at the center
of the swirl chamber 8, thereby making the most of the air ejected
through the sub-nozzle holes 12 and causing effective swirls in the
15 swirl chamber 8.

20 【0027】 Fig. 1A shows, as a preferred embodiment, that the center
12c of the open end of each sub-nozzle hole 12 overlaps the sphere
15 having a radius of 50% when the mouthpiece 7 is seen from just
above, thereby enabling the central axis 12a-12b of each sub-nozzle
hole 12 to pass through the center of the swirl chamber 8. In this
case, the radius is preferably 70%, more preferably 60%, and most
preferably 50% of that (100%) of the open end of the top-open recess
7b.

25 【0028】 In Figs. 1A and 1D, a hypothetical reference line 16
extends just upwards. The position of each hole 12 is determined

in relation to this hypothetical reference line 16; that is, each sub-nozzle hole 12 is positioned such that its central axis 12a-12b coincides with the reference line 16 in every direction as viewed in Figs. 1A to 1D.

5 **【0029】** In this way the sub-nozzle holes 12 are positioned at various angles for the reference line 16 (Figs. 1B and 1D). If it is positioned at a relatively small angle to the reference line 16, the sub-nozzle hole 12 can be short in length, thereby reducing frictional resistance to the flow of a secondary air passing through
10 the sub-nozzle hole. In Fig. 1B where the cross-section of the mouthpiece 7 is viewed from the side, and the two sub-nozzle holes 12 appear to be in alignment, the central axis 12a-12b of the sub-nozzle hole 12 is preferably inclined at 30° or less to the reference line 16, which will be referred to as “first angle”. In
15 Fig. 1D where the cross-section of the mouthpiece 7 is viewed from the back, and the sub-nozzle holes 12 appear to be arranged side by side, the central axis 12a-12b is preferably inclined at 15° which will be referred to as “second angle”. In another preferred embodiment the first angle is 15° or less, and the second angle is 8°
20 or less; more preferably, 8° or less to 4° or less, and most preferably, 4° or less to 2° or less.

【0030】 In the embodiment illustrated in Figs. 1B and 1C the first angle is 30° and the second angle is 15° each angular relation being indicated by chain lines.

25 **【0031】** The size of each sub-nozzle hole 12 is determined as

follows:

It has been demonstrated that when the main nozzle hole 11 has an open end having an effective area is supposed to be 100%, the total area of the open ends of the two sub-nozzle holes should
5 be in the range of 3% to 15%; preferably, 4 to 10%; more preferably, 6 to 10%, and most preferably, 7 to 9%. In short, the range of 3 to 15%, or preferably, of 5 to 15% is effective to reduce the production of NO_x and fumes evenly.

[0032] The main nozzle hole 11 is constructed as follows:

10 Referring to Figs. 2A to 2D, the main nozzle hole 11 includes a main groove 17 and a pair of side grooves 18 communicatively continuous to the main groove 17 through banks (not numbered). In Fig. 2A, each side groove 18 is formed such that its central axis 18a is slightly behind the central axis 17a of the main groove 17.
15 Each side groove 18 is also arranged that its angle of elevation is smaller than 45° of the axis 17a.

[0033] As best shown in Fig. 1A, each of the side grooves 18 gradually but slightly becomes narrower in width toward the depth of the main nozzle hole 11 while the main groove 17 remains the
20 same along its full length. The side grooves are positioned such that the distance between them diminishes toward their forward ends. Each of the side grooves has a progressively diminishing cross-sectional area toward its forward end. When the mouthpiece is seen from just above, each of the side grooves is arranged at a
25 position retreated from an upper opening of every sub-nozzle hole in

parallel to a center axis of the main nozzle hole and immediately rearwards thereof.

5 【0034】 Referring Figs. 4 and 5, the major advantage of the first embodiment is that environmental contaminants such as NO_x and fumes are reduced in the exhaust gases, which will be demonstrated, on condition that the applied load is the same:

10 【0035】 From Fig. 4, it will be understood that the first embodiment has less nitrogen oxides (NO_x) than a contrasted example (1) that has neither sub-nozzle holes 12 nor the side grooves 18. It will be appreciated that the sub-nozzle holes 12 and the side grooves 18 are effective to reduce NO_x content.

15 【0036】 Fig. 5 shows that the first embodiment has less NO_x and less fumes than contrasted examples 1 and 2, wherein the contrasted example 2 has sub-nozzle holes corresponding to the sub-nozzle holes 12 but no grooves corresponding to the side grooves 18. The comparison between the contrasted examples 1 and 2 shows that the addition of the secondary air sub-nozzle holes 12 are conducive to the reduction of NO_x and fumes. Likewise, the comparison between the first embodiment and the contrasted
20 example 2 shows that the side grooves 18 are conducive to the reduction of NO_x and fumes.

25 【0037】 The efficiency of reducing exhaust gases depends upon the area of the open end of the sub-nozzle hole 12. Referring to Fig. 6A to 6C, each horizontal co-ordinate is the percentage of the total minimum area of the open ends of the sub-nozzle holes 12 to the

area of the open end of the main nozzle hole 11. The vertical co-ordinate of Fig. 6A indicates variations in the amount of NO_x; in Fig. 6B the vertical co-ordinate indicates variations in the amount of fumes, and in Fig. 6C the vertical co-ordinate indicates variations in the total amount of NO_x and fumes. Each coefficient of variation is calculated, as a reference value, based upon the amount of NO_x and fumes produced in the combustion chamber having no sub-nozzle holes 12. Let the reference value be α , and the amount of variation be β . Then, the coefficient of variation will be $(\beta - \alpha)/\alpha$.

【0038】 As shown in Fig. 6C, the absolute value of the total reduction rate is maximized when the area of the open end of the sub-nozzle holes 12 is 7.7%. Let the absolute value of the reduction rate at this stage be 100%. It has been demonstrated that to increase the rate of reduction of exhaust gases up to 98%, the total area of the open ends of the sub-nozzle hole 12 must be in the range of 7 to 9%, and if it exceeds 95%, the total area can be in the range of 6 to 10%. If it exceeds 60%, the total area can be in the range of 3 to 15%. Among these ranges, when it exceeds 70%, and both NO_x and fumes effectively decrease, the total area is in the range of 4 to 10%. As a result, it will be concluded that the total area of the open ends of the sub-nozzle holes preferably in the range of 3 to 15%; more preferably, 4 to 10%, further preferably, 6 to 10%, and most preferably, 7 to 9%.

【0039】 Referring to Figs. 7, 8 and 9, a second embodiment, a third

embodiment and a fourth embodiment will be described,
respectively:

5 【0040】 In the second embodiment shown in Fig. 7 the total area of
the open ends of the sub-nozzle holes 12 is 8% of the area (100%) of
the open end of the main nozzle hole 11, wherein each sub-nozzle
hole has an open end having the same area. This embodiment
reduces the production of NOx or fumes or both, as clearly
demonstrated by comparison with the contrasted examples 1 and 2.

10 【0041】 In the third embodiment shown in Fig. 8 the pair of
sub-nozzle holes 12 are inclined forwardly and upwardly toward the
swirl chamber 8 or, in other words, slightly converged toward the
swirl chamber 8 from the combustion chamber 9 in contrast to the
first and second embodiments where they extend upright between
the combustion chamber 9 and the swirl chamber 8. In Fig. 8B the
15 angle of incline is 30° and in Fig. 8D, the angle of incline is 15°
toward each other.

20 【0042】 In the fourth embodiment shown in Fig. 9A to 9D, the pair
of sub-nozzle holes 12 are inclined rearwardly and upwardly toward
the swirl chamber 8, as best shown in Fig. 9B, and, as shown in Fig.
9D, are inclined outwardly or, in other words, slightly diverged
toward the swirl chamber 8 from the combustion chamber 9. In Fig.
9B the angle of incline is 30° and in Fig. 9D, the angle of incline is
15° toward each other.